APPENDIX 11-2

CARBON CALCULATIONS

Core input data

ENTER INPUT DATA HERE! VALUES SHOULD ONLY BE CHANGED ON THIS SHEET. **DO NOT USE EXAMPLE VALUES AS DEFAULTS!** ENTER YOUR OWN VALUES THAT ARE SPECIFIC TO YOUR PARTICULAR SITE.

Note: The input parameters include some variables that can be specified by default values, but others that must be site specific. Variables that can be taken from defaults are marked with purple tags on left hand side.

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Input data	Expected values: Enter expected value here	Record source of data	Possible range of values: Enter minimum value here	Record source of data	Possible range of values: Enter maximum value here	Record source of data
Windfarm characteristics						
Dimensions						
No. of turbines	9		9		9	
Lifetime of windfarm (years)	35	Fixed	35		35	
Performance						
Power rating of turbines (turbine capacity) (MW)	7		6.9		7.1	
Capacity factor	Direct input of capacity fac		Direct input of capacity fac		Direct input of capacity fac	
Enter estimated capacity factor (percentage efficiency)	0.35		0.35		0.350	
Backup						
Extra capacity required for backup (%)	5		5		5	
Additional emissions due to reduced thermal efficiency of the reserve generation (%)	10		10		10	
Carbon dioxide emissions from turbine life - (eg. manufacture, construction, decommissioning)	Calculate wrt installed cap		Calculate wrt installed cap		Calculate wrt installed cap	
Characteristics of peatland before windfarm development						
Type of peatland	Acid b		Acid b		Acid b	
Average annual air temperature at site (^oC)	9.27		4.6		15	
Average depth of peat at site (m)	1.30		1.30		1.30	
C Content of dry peat (% by weight)	53.23		19.57		64.28	
Average extent of drainage around drainage features at site (m)	15.00		15.00		15.00	
Average water table depth at site (m)	0.50		0.10		1.00	
Dry soil bulk density (g cm^{-3})	0.132		0.072		0.293	
Characteristics of bog plants						
Time required for regeneration of bog plants after restoration (years)	10		5		15	
Carbon accumulation due to C fixation by bog plants in undrained peats (tC ha^{-1} yr^{-1})	0.25		0.2		0.3	
Forestry Plantation Characteristics						
Method used to calculate CO_2 loss from forest felling	Enter simple data		Enter simple data		Enter simple data	
Area of forestry plantation to be felled (ha)	11.25		11.25		11.25	
Average rate of carbon sequestration in timber (tC ha-1 yr-1)	3.45		3.50		3.55	
Counterfactual emission factors						
To update counterfactual emission factors from the web Click here (not yet operational)						
Coal-fired plant emission factor (t CO_2 MWh^{-1})	0.945		0.945		0.945	
Grid-mix emission factor (t CO_2 MWh^{-1})	0.207		0.207		0.207	
Fossil fuel-mix emission factor (t CO_2 MWh^{-1})	0.424		0.424		0.424	
Borrow pits						
Number of borrow pits	0		0		0	
Average length of pits (m)	0		0		0	
Average width of pits (m)	0		0		0	
Average depth of peat removed from pit (m)	0.00		0.00		0.00	
Foundations and hard-standing area associated with each turbine						
Method used to calculate CO_2 loss from foundations and hard-standing	Rectangular with vertical w		Rectangular with vertical w		Rectangular with vertical w	
Average length of turbine foundations (m)	25		25		25	
Average width of turbine foundations (m)	25		25		25	
Average depth of peat removed from turbine foundations (m)	1.30		1.30		1.30	
Average length of hard-standing (m)	97		97		97	
Average width of hard-standing (m)	35		35		35	
Average depth of peat removed from hard-standing (m)	1.30		1.30		1.30	
Access tracks						
Total length of access track (m)	10550		10550		10550	
Existing track length (m)	1250		1250		1250	
Length of access track that is floating road (m)	2100		2100		2100	
Floating road width (m)	5		5		5	
Floating road depth (m)						
Length of floating road that is drained (m)						
Average depth of drains associated with floating roads (m)						
Length of access track that is excavated road (m)	7200		7200		7200	
Excavated road width (m)	5		5		5	
Average depth of peat excavated for road (m)	1.30		1.30		1.30	
Length of access track that is rock filled road (m)						
Rock filled road width (m)						
Rock filled road depth (m)						
Length of rock filled road that is drained (m)						
Average depth of drains associated with rock filled roads (m)						
Cable Trenches						
Length of any cable trench on peat that does not follow access tracks and is lined with a permeable medium (eg. sand) (m)						
Average depth of peat cut for cable trenches (m)	1.20		1.20		1.20	
Additional peat excavated (not already accounted for above)						
Volume of additional peat excavated (m^3)	4110		4110		4110	
Area of additional peat excavated (m^2)	34800.0		34800.0		34800.0	
Peat Landslide Hazard	Negligible		Negligible		Negligible	
Weblink: Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments						
Improvement of C sequestration at site by blocking drains, restoration of habitat etc						
Improvement of degraded bog						
Area of degraded bog to be improved (ha)						
Water table depth in degraded bog before improvement (m)						
Water table depth in degraded bog after improvement (m)						
Time required for hydrology and habitat of bog to return to its previous state on improvement (years)						
Period of time when effectiveness of the improvement in degraded bog can be guaranteed (years)	25		25		25	
Improvement of felled plantation land						
Area of felled plantation to be improved (ha)						
Water table depth in felled area before improvement (m)						
Water table depth in felled area after improvement (m)						
Time required for hydrology and habitat of felled plantation to return to its previous state on improvement (years)						
Period of time when effectiveness of the improvement in felled plantation can be guaranteed (years)	25		25		25	
Restoration of peat removed from borrow pits						
Area of borrow pits to be restored (ha)						
Depth of water table in borrow pit before restoration with respect to the restored surface (m)						
Depth of water table in borrow pit after restoration with respect to the restored surface (m)						
Time required for hydrology and habitat of borrow pit to return to its previous state on restoration (years)						
Period of time when effectiveness of the restoration of peat removed from borrow pits can be guaranteed (years)	25		25		25	
Early removal of drainage from foundations and hardstanding						
Water table depth around foundations and hardstanding before restoration (m)						
Water table depth around foundations and hardstanding after restoration (m)	15.00		15.00		15.00	
Time to completion of backfilling, removal of any surface drains, and full restoration of the hydrology (years)						
Restoration of site after decomissioning						
Will the hydrology of the site be restored on decommissioning?	No		No		No	
Will you attempt to block any gullies that have formed due to the windfarm?	No		No		No	
Will you attempt to block all artificial ditches and facilitate rewetting?	No		No		No	
Will the habitat of the site be restored on decommissioning?	No		No		No	
Will you control grazing on degraded areas?	No		No		No	
Will you manage areas to favour reintroduction of species	No		No		No	

Choice of methodology for calculating emission factors	Site specific (required for planning applications)

Note: Capacity factor. The capacity factor of any power plant is the proportion of energy produced during a given period with respect to the energy that would have been produced had the wind farm been running continually and at maximum output (DECC (2004); see also www.bwea.com/ref/capacityfactors.html).
Capacity Factor = Electricity generated during the period [kWh]/ (Installed capacity [kW] x number of hours in the period [h])
We recommend that a site-specific capacity factor ~~site~~ should be used (as measured during planning stage), and should represent the average emission factor expected over the lifetime of the windfarm, accounting for decline in efficiency with age (Hughes, 2012). The 5 year average capacity factor (or "load factor") for UK onshore wind between 2010 and 2014, based on average beginning and end of year capacity, was 29.2% (DUKES, 2015).

Note: Extra capacity required for backup. If 20% of national electricity is generated by wind energy, the extra capacity required for backup is 5% of the rated capacity of the wind plant (Dale et al 2004). We suggest this should be 5% of the actual output. If it is assumed that less than 20% of national electricity is generated by wind energy, a lower percentage should be entered (0%). The House of Lords Economic Affairs Committee report on The Economics of Renewable Energy (Parliamentary Business, 2008) notes that to cover peak demand a '20% margin of extra capacity has been sufficient to keep the risk of a power cut due to insufficient generation at a very low level.' The estimate provided by BERR was a range of 10% to 20% of installed capacity of wind energy. E.ON is reported as proposing that the capacity credit of wind power should be 8%, and The Renewable Energy Foundation proposed the use of the square root of the wind capacity (in GW) as conventional capacity (e.g. 36 GW of wind plant to match 6 GW of conventional plant).

Note: Extra emissions due to reduced thermal efficiency of the reserve power generation ≈ 10%

Note: Emissions from turbine life. If total emissions for the windfarm are unknown, emissions should be calculated according to turbine capacity. The normal range of CO_2 emissions is 394 to 8147 t CO_2 MW (White & Kulcinski, 2000; White, 2007).

Note: Type of peatland An 'acid bog' is fed primarily by rainwater and often inhabited by sphagnum moss, thus making it acidic (Stoneman & Brooks,1997).
A 'fen' is a type of wetland fed by surface and/or groundwater (McBride et al., 2011).

Note: Time required for regeneration of previous habitat. Loss of fixation should be assumed to be over lifetime of windfarm only. This time could be longer if plants do not regenerate. The requirements for after-use planning include the provision of suitable refugia for peat-forming vegetation, the removal of structures, or an assessment of the impact of leaving them in situ. Methods used to reinstate the site will affect the likely time for regeneration of the previous habitat. This time could also be shorter if plants regenerate during lifetime of windfarm. If so, enter number of years estimated for regeneration.

Note: Carbon fixation by bog plants
Apparent C accumulation rate in peatland is 0.12 to 0.31 t C ha^{-1} yr^{-1} (Turunen et al., 2001; Botch et al., 1995). The SNH guidance uses a value of 0.25 t C ha^{-1} yr^{-1}.

Note: Area of forestry plantation to be felled. If the forestry was planned to be removed, with no further rotations planted, before the windfarm development, the area to be felled should be entered as zero.

Note: Plantation carbon sequestration. This is dependent on the yield class of the forestry. The SNH technical guidance assumed yield class of 16 m^3 ha^{-1} yr^{-1}, compared to the value of 14 m^3 ha^{-1} yr^{-1} provided by the Forestry Commission. Carbon sequestered for yield class 16 m^3 ha^{-1} y^{-1} = 3.6 tC ha^{-1} yr^{-1} (Cannell, 1999).

Note: Coal-Fired Plant and Grid Mix Emission Factors. Coal-fired plant emission factor (EF) from electricity supplied in 2014 = 0.093 t CO_2 MWh^{-1}; Grid-Mix EF for 2014 = 0.394 t CO_2 MWh^{-1}. Source = DUKES, 2015b.

Note: Fossil Fuel-Mix Emission Factor. The emission factor from electricity supplied in 2014 from all fossil fuels = 0.642 t CO_2 MWh^{-1}. Source = DUKES, 2015b.

Note: Total length of access track. If areas of access track overlap with hardstanding area, exclude these from the total length of access track to avoid double counting of land area lost.

Note: Floating road depth. Accounts for sinking of floating road. Should be entered as the average depth of the road expected over the lifetime of the windfarm. If no sinking is expected, enter as zero.

Note: Length of floating road that is drained. Refers to any drains running along the length of the road.

Note: Rock filled roads. Rock filled roads are assumed to be roads where no peat has been removed and rock has been placed on the surface and allowed to settle.

Note: Depth of peat cut for cable trenches. In shallow peats, the cable trenches may be cut below the peat. To avoid overestimating the depth of peat affected by the cable trenches, only enter the depth of the peat that is cut.

Note: Peat Landslide Hazard. It is assumed that measures have been taken to limit damage (Scottish Executive, 2006, Peat Landslide Hazard and Risk Assessments. Best Practice Guide for Proposed Electricity Generation Developments. Scottish Executive, Edinburgh. pp. 34-35) so that C losses due to peat landslide can be assumed to be negligible. Link: http://www.scotland.gov.uk/Publications/2006/12/21162303/1.

Note: Period of time when improvement can be guaranteed. This guarantee should be absolute. Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong supporting evidence that this improvement can be guaranteed for the full period given. This includes the time requirement for the improvement to become effective. For example if time required for hydrology and habitat to return to its previous state is 10 years and the restoration can be guaranteed over the lifetime of the windfarm (25 years), the period of time when the improvement can be guaranteed should be entered as 25 years, and the improvement will be effective for (25 -10) = 15 years.

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Note: Period of time when improvement can be guaranteed. This is assumed to be the lifetime of the windfarm as restoration after windfarm decommissioning is already accounted for in restoration of the site

Note: Restoration of site. If the water table at the site is returned to its original level or higher on decommissioning, and habitat at the site is restored, it is assumed that C losses continue only over the lifetime of the windfarm. Otherwise, C losses from drained peat are assumed to be 100%.

Note: Choice of methodology for calculating emission factors. The IPCC default methodology is the internationally accepted standard (IPCC, 1997). However, it is stated in IPCC (1997) that these are rough estimates, and "these rates and production periods can be used if countries do not have more appropriate estimates". Therefore, we have developed more site specific estimates for use here based on work from the Scottish Government funded ECOSSE project (Smith et al, 2007. ECOSSE: Estimating Carbon in Organic Soils - Sequestration and Emissions. Final Report. SEERAD Report. ISBN 978 0 7559 1498 2. 166pp.).

Core input data

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Results

PAYBACK TIME AND CO_2 EMISSIONS

Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

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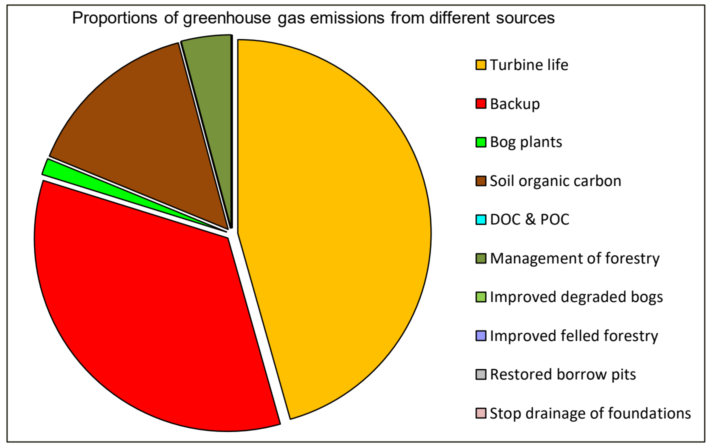
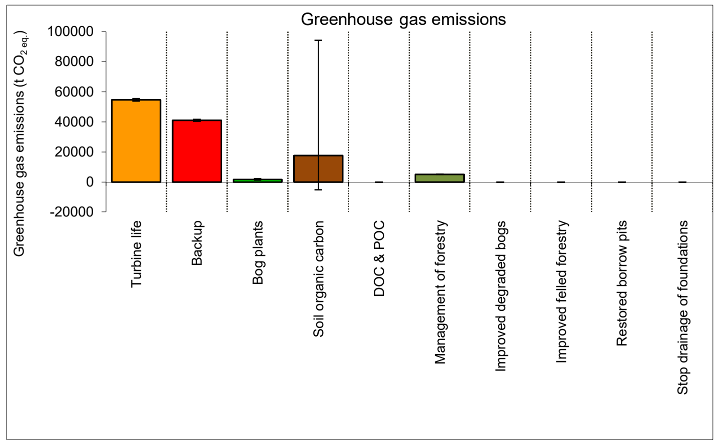
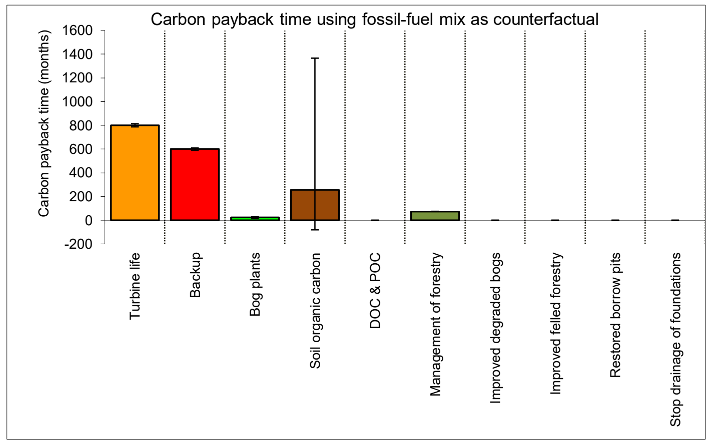
	Exp.	Min.	Max.
1. Windfarm CO_2 emission saving over…			
…coal-fired electricity generation (tCO_2 yr^{-1})	1825	1799	1851
…grid-mix of electricity generation (tCO_2 yr^{-1})	400	394	406
…fossil fuel - mix of electricity generation (tCO_2 yr^{-1})	819	807	831
Energy output from windfarm over lifetime (MWh)	67605	66640	68571
Total CO_2 losses due to wind farm (t CO_2 eq.)			
2. Losses due to turbine life (eg. manufacture, construction, decomissioning)	54656	53815	55497
3. Losses due to backup	40949	40365	41534
4. Losses due to reduced carbon fixing potential	1656	1177	2208
5. Losses from soil organic matter	17555	-5161	94267
6. Losses due to DOC & POC leaching	0	0	0
7. Losses due to felling forestry	4981	5054	5126
Total losses of carbon dioxide	119798	95250	198632
8. Total CO_2 gains due to improvement of site (t CO_2 eq.)			
8a. Change in emissions due to improvement of degraded bogs	0	0	0
8b. Change in emissions due to improvement of felled forestry	0	0	0
8c. Change in emissions due to restoration of peat from borrow pits	0	0	0
8d. Change in emissions due to removal of drainage from foundations & hardstanding	0	0	0
Total change in emissions due to improvements	0	0	0

RESULTS	Exp.	Min.	Max.
Net emissions of carbon dioxide (t $CO_{2\ eq.}$)	**119798**	**95250**	**198632**
Carbon Payback Time			
…coal-fired electricity generation (years)	65.6	51.4	110.4
…grid-mix of electricity generation (years)	299.6	234.9	504.0
…fossil fuel - mix of electricity generation (years)	**146.3**	**114.7**	**246.0**
Ratio of soil carbon loss to gain by restoration (TARGET ratio (Natural Resources Wales) < 1.0)	**No gains!**	**No gains!**	**No gains!**
Ratio of CO_2 eq. emissions to power generation (g / kWh) (TARGET ratio by 2030 (electricity generation) < 50 g /kWh)	**1772**	**1389**	**2981**







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Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greenhouse gas emissions

	Exp.	Min	Max
Turbine life	54656	841	841
Backup	40949	585	585
Bog plants	1656	478	552
Soil organic carbon	17555	22716	76712
DOC & POC	0	0	0
Management of forestry	4981	0	144
Improved degraded bogs	0	0	0
Improved felled forestry	0	0	0
Restored borrow pits	0	0	0
Stop drainage of foundations	0	0	0

Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greenhouse gas emissions				Carbon payback time (months)		
	Exp.	Min.	Max.	Exp.	Min.	Max.
Turbine life	54656	841	841	801	12	12
Backup	40949	585	585	600	9	8
Bog plants	1656	478	552	24	7	8
Soil organic carbon	17555	22716	76712	257	338	1108
DOC & POC	0	0	0	0	0	0
Management of forestry	4981	-72	144	73	-1	2
Improved degraded bogs	0	0	0	0	0	0
Improved felled forestry	0	0	0	0	0	0
Restored borrow pits	0	0	0	0	0	0
Stop drainage of foundations	0	0	0	0	0	0
	119798			1755		

Results

PAYBACK TIME AND CO_2 EMISSIONS

Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

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Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine life with carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

Method used to estimate CO_2 emissions from turbine life (eg. manufacture, construction,	Calculate wrt installed capacity

	Exp	Min	Max
Direct input of emissions due to turbine life (t CO_2 windfarm^{-1})	**0**	**0**	**0**
Calculation of emissions due to turbine life from energy output			
CO_2 emissions due to turbine life (tCO_2 turbine^{-1})	6073	5979	6166
No. of turbines	9	9	9
Total calculated CO_2 emission of the wind farm due to turbine life (t CO_2 windfarm^{-1})	54656	53815	55497

	Total			Construction Area 1			Construction Area 2			Construction Area 3			Construction Area 4			Construction Area 5		
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Calculation of emissions due to cement used in construction																		
Volume of cement used (m^3)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
CO_2 emission rate (t CO_2 m^{-3} cement)	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316
Total CO_2 emissions due to cement used	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

RESULTS			
Losses due to turbine life (eg.	54656	53815	55497
Additional CO_2 payback time of windfarm due to turbine life (eg. manufacture, contruction, decomissioning)			
…coal-fired electricity generation (months)	359	359	360
…grid-mix of electricity generation (months)	1640	1639	1642
…fossil fuel - mix of electricity generation (months)	801	800	802

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Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine life with carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

http://www.concretecentre.com/PDF/SCF_Table%207%20Embodied%20CO2_April%202013.pdf

mpa The Concrete Centre

Embodied carbon dioxide (CO_2e) of concretes used in buildings

CONCRETE APPLICATION	Concrete designation	CO_2e ($kgCO_2e/m^3$)[1] CEM I concrete	30% fly ash concrete	50% ggbs concrete	CO_2e ($kgCO_2e$/tonne)[1] CEM I concrete	30% fly ash concrete	50% ggbs concrete
Blinding, mass fill, strip footings, mass foundations, trench foundations [2]	GEN1	177	128	101	77	55	44
Reinforced Foundations [2]	RC25/30**	316	263	197	133	111	83
Ground floors [2]	RC28/35 *	316	261	186	134	110	79
Structural: in situ floors, superstructure, walls, basements [2]	RC32/40 **	369	313	231	154	131	96
High strength concrete [2]	RC40/50 **	432	351	269	178	146	111
		CO_2e ($kgCO_2e/m^3$)			CO_2e ($kgCO_2e$/tonne)		
Unreinforced Precast flooring[3]		-			165		
Reinforced precast flooring[3]		-			171		
Average Generic Concrete Block[4]		-			84		

* includes 30kg/m^3 steel reinforcement

** includes 100kg/m^3 steel reinforcement

Emissions due to backup power generation

Note: CO_2 loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

	Expected	Minimum	Maximum
Reserve capacity required for backup			
No. of turbines	9	9	9
Power rating of turbines (turbine capacity) (MW)	7	6.9	7.1
Power of wind farm (MW h^{-1})	63	62.1	63.9
Rated capacity (MW yr^{-1})	551880	543996	559764
Extra capacity required for backup (%)	5	5	5
Additional emissions due to reduced thermal efficiency of the reserve generation (%)	10	10	10
Reserve capacity (MWh yr^{-1})	2759	2720	2799

	Expected	Minimum	Maximum
Carbon dioxide emissions due to backup power generation			
Coal-fired plant emission factor (t CO_2 MWh^{-1})	0.945	0.945	0.945
Grid-mix emission factor (t CO_2 MWh^{-1})	0.207	0.207	0.207
Fossil fuel- mix emission factor (t CO_2 MWh^{-1})	0.424	0.424	0.424
Lifetime of windfarm (years)	35	35	35
Annual emissions due to backup from…			
…coal-fired electricity generation (tCO_2 yr^{-1})	2608	2570	2645
…grid-mix of electricity generation (tCO_2 yr^{-1})	571	563	579
…fossil fuel - mix of electricity generation (tCO_2 yr^{-1})	1170	1153	1187

	Expected	Minimum	Maximum
RESULTS			
Total emissions due to backup from…			
…coal-fired electricity generation (tCO_2)	91267	89963	92571
…grid-mix of electricity generation (tCO_2)	19992	19706	20277
…fossil fuel - mix of electricity generation (tCO_2)	**40949**	**40365**	**41534**
Additional CO_2 payback time of windfarm due to backup			
…coal-fired electricity generation (months)	600	600	600
…grid-mix of electricity generation (months)	600	600	600
…fossil fuel - mix of electricity generation (months)	600	600	600

Assumption: Backup assumed to be by fossil-fuel-mix of electricity generation. Note that hydroelectricity may also be used for backup, so this assumption may make the value for backup generation too high. These assumptions should be revisited as technology develops.

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Emissions due to backup power generation

Note: CO_2 loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

Note: Wind generated electricity is inherently variable, providing unique challenges to the electricity generating industry for provision of a supply to meet consumer demand (Netz, 2004). Backup power is required to accompany wind generation to stabilise the supply to the consumer. This backup power will usually be obtained from a fossil fuel source. At a high level of wind power penetration in the overall generating mix, and with current grid management techniques, the capacity for fossil fuel backup may become strained because it is being used to balance the fluctuating consumer demand with a variable and highly unpredictable output from wind turbines (White, 2007). The Carbon Trust (Carbon Trust/DTI, 2004) concluded that increasing levels of intermittent generation do not present major technical issues at the percentages of renewables expected by 2010 and 2020, but the UK renewables target at the time of that report was only 20%. When national reliance on wind power is low (less than ~20%), the additional fossil fuel generated power requirement can be considered to be insignificant and may be obtained from within the spare generating capacity of other power sectors (Dale et al, 2004). However, as the national supply from wind power increases above 20%, without improvements in grid management techniques, emissions due to backup power generation may become more significant. The extra capacity needed for backup power generation is currently estimated to be 5% of the rated capacity of the wind plant if wind power contributes more than 20% to the national grid (Dale et al 2004). Moving towards the SG target of 50% electricity generation from renewable sources, more short-term capacity may be required in terms of pumped-storage hydro-generated power, or a better mix of offshore and onshore wind generating capacity. Grid management techniques are anticipated to reduce this extra capacity, with improved demand side management, smart meters, grid reinforcement and other developments. However, given current grid management techniques, it is suggested that 5% extra capacity should be assumed for backup power generation if wind power contributes more than 20% to the national grid. At lower contributions, the extra capacity required for backup should be assumed to be zero. These assumptions should be revisited as technology improves.

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

	Expected	Minimum	Maximum
Area where carbon accumulation by bog plants is lost			
Total area of land lost due to windfarm construction (m^2)	117480	117480	117480
Total area affected by drainage due to windfarm construction (m^{-2})	283866	283866	283866
Total area where fixation by plants is lost (m^2)	401346	401346	401346

Assumptions:
1. Bog plants are 100% lost from the area where peat is removed for construction.
2. Bog plants are 100% lost from the area where peat is drained.
3. The recovery of carbon accumulation by plants on restoration of land is as given in inputs.

	Expected	Minimum	Maximum
Total loss of carbon accumulation			
Carbon accumulation in undrained peats (tC ha^{-1} yr^{-1})	0.25	0.2	0.3
Lifetime of windfarm (years)	35	35	35
Time required for regeneration of bog plants after restoration (years)	10	5	15
Carbon accumulation up to time of restoration (tCO_2 eq. ha^{-1})	41	29	55

	Expected	Minimum	Maximum
RESULTS			
Total loss of carbon accumulation by bog plants			
Total area where fixation by plants is lost (ha)	40	40	40
Carbon accumulation over lifetime of windfarm (tCO_2 eq. ha^{-1})	41	29	55
Total loss of carbon fixation by plants at the site (t CO_2)	**1656**	**1177**	**2208**
Additional CO_2 payback time of windfarm due to loss of CO2 fixing potential			
…coal-fired electricity generation (months)	11	8	14
…grid-mix of electricity generation (months)	50	36	65
…fossil fuel - mix of electricity generation (months)	24	18	32

Click here to move to Payback Time Click here

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO_2 loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

		Expected result	Minimum result	Maximum result
	CO_2 loss due to windfarm construction			
Check	CO_2 loss from removed peat (t CO_2 equiv)	14828	-5161	58064
Check	CO_2 loss from drained peat (t CO_2 equiv)	2728	0	36203
	RESULTS			
	Total CO_2 loss from peat (removed + drained) (t CO_2 equiv)	**17555**	**-5161**	**94267**
	Additional CO_2 payback time of windfarm due to loss of soil CO2			
	…coal-fired electricity generation (months)	115	-34	611
	…grid-mix of electricity generation (months)	527	-157	2789
	…fossil fuel - mix of electricity generation (months)	257	-77	1362

Click here to move to Payback Time Click here

Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO_2 loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

Volume of Peat Removed

Note: % site lost by peat removal is estimated from peat removed in borrow pits, turbine foundations, hard-standing and access tracks.
If peat is removed for any other reason, this must be added in as additional peat excavated in the core input sheet.

Peat removed from borrow pits	Total Exp	Min	Max
Number of borrow pits	0	0	0
Average length of pits (m)	0	0	0
Average width of pits (m)	0	0	0
Average depth of peat removed from pit (m)	0	0	0
Area of land lost in borrow pits (m^2)	0	0	0
Volume of peat removed from borrow pits (m^3)	0	0	0

Peat removed from turbine foundations	Total Exp	Min	Max	Construction Area 1 Exp	Min	Max	Construction Area 2 Exp	Min	Max	Construction Area 3 Exp	Min	Max	Construction Area 4 Exp	Min	Max	Construction Area 5 Exp	Min	Max
Method used to calculate CO_2 loss from foundations	Rectangular with vertical walls																	
Calculation method code		1																
No. of turbines	9	9	9	9	9	9	0	0	0	0	0	0	0	0	0	0	0	0
Diameter at surface (m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
Diameter at bottom (m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
Depth of foundations (m)				1	1	1	0	0	0	0	0	0	0	0	0	0	0	0
"Area" of land lost in hard-standing (m^2)	5625	5625	5625	5625	5625	5625	0	0	0	0	0	0	0	0	0	0	0	0
Volume of peat removed from foundation area (m^3)	7312.5	7312.5	7312.5	7312.5	7312.5	7312.5	0	0	0	0	0	0	0	0	0	0	0	0

Peat removed from hard-standing	Exp	Min	Max	Construction Area 1 Exp	Min	Max	Construction Area 2 Exp	Min	Max	Construction Area 3 Exp	Min	Max	Construction Area 4 Exp	Min	Max	Construction Area 5 Exp	Min	Max
Method used to calculate CO_2 loss from foundations	Rectangular with vertical walls																	
Calculation method code		1																
No. of turbines	9	9	9	9	9	9	0	0	0	0	0	0	0	0	0	0	0	0
Diameter at surface (m)				97	97	97	0	0	0	0	0	0	0	0	0	0	0	0
				35	35	35	0	0	0	0	0	0	0	0	0	0	0	0
Diameter at bottom (m)				97	97	97	0	0	0	0	0	0	0	0	0	0	0	0
				35	35	35	0	0	0	0	0	0	0	0	0	0	0	0
Depth of hardstanding (m)				1	1.3	1.3	0	0	0	0	0	0	0	0	0	0	0	0
Area of land lost in hard-standing (m^2)	30555	30555	30555	30555	30555	30555	0	0	0	0	0	0	0	0	0	0	0	0
Volume of peat removed from hardstandingarea (m^3)	39722	39722	39722	39722	39722	39722	0	0	0	0	0	0	0	0	0	0	0	0

Peat removed from access tracks	Total Exp	Min	Max
Floating roads			
Length of access track that is floating road (m)	2100	2100	2100
Floating road width (m)	5	5	5
Floating road depth (m)	0	0	0
Area of land lost in floating roads (m^2)	10500	10500	10500
Volume of peat removed for floating roads	0	0	0
Excavated roads			
Length of access track that is excavated road (m)	7200	7200	7200
Excavated road width (m)	5	5	5
Average depth of peat excavated for road (m)	1.3	1.3	1.3
Area of land lost in excavated roads (m^2)	36000	36000	36000
Volume of peat removed for excavated roads	46800	46800	46800
Rock-filled roads			
Length of access track that is rock filled road (m)	0	0	0
Rock filled road width (m)	0	0	0
Rock filled road depth (m)	0	0	0
Area of land lost in excavated roads (m^2)	0	0	0
Volume of peat removed for rock-filled roads	0	0	0
Total area of land lost in access tracks (m^2)	46500	46500	46500
Total volume of peat removed due to access tracks (m^3)	46800	46800	46800

Additional peat excavated - (not already accounted for above)			
Volume of additional peat excavated (m^3)	4110	4110	4110
Area of additional peat excavated (m^2)	34800	34800	34800

RESULTS	Total Exp	Min	Max
Total volume of peat removed (m^3) due to windfarm construction	**97944**	**97944**	**97944**
Total area of land lost due to windfarm construction (m^2)	**117480**	**117480**	**117480**

Click here to move to 5b. CO2 loss from removed peat — Click here

Click here to move to Payback Time — Click here

Volume of Peat Removed

Note: % site lost by peat removal is estimated from peat removed in borrow pits, turbine foundations, hard-standing and access tracks.
If peat is removed for any other reason, this must be added in to the volume of peat removed, area of land lost and % site lost at the bottom of this worksheet.

CO_2 loss from removed peats

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

	Expected	Minimum	Maximum
CO_2 loss from removed peat			
C Content of dry peat (% by weight)	53.23	19.57	64.28
Dry soil bulk density (g cm^{-3})	0.13	0.07	0.29
% C contained in removed peat that is lost as CO_2	100	100	100
Total volume of peat removed (m^3) due to windfarm construction	97944	97944	97944
CO_2 loss from removed peat (t CO_2)	25236	5061	67644

Check

Assumption: If peat is not restored, 100% of the carbon contained in the removed peat is lost as CO_2

CO_2 loss from undrained peat left in situ			
Total area of land lost due to windfarm construction (ha)	12	12	12
CO_2 loss from undrained peat left in situ (t CO_2 ha^{-1})	886	870	815
CO_2 loss from undrained peat left in situ (t CO_2)	10408	10221	9580

CO_2 loss attributable to peat removal only			
CO_2 loss from removed peat (t CO_2)	25236	5061	67644
CO_2 loss from undrained peat left in situ (t CO_2)	10408	10221	9580
RESULTS			
CO_2 loss attributable to peat removal only (t CO_2)	**14828**	**-5161**	**58064**

Click here to move to 5. Loss of soil CO_2 Click here

Click here to move to Payback Time Click here

CO_2 loss from removed peats

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

Volume of peat drained

Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

Extent of drainage around each metre of drainage ditch	Total Exp	Total Min	Total Max
Average extent of drainage around drainage features at site (m)	15	15	15

Peat affected by drainage around borrow pits	Total Exp	Total Min	Total Max
Number of borrow pits	0	0	0
Average length of pits (m)	0	0	0
Average width of pits (m)	0	0	0
Average depth of peat removed from pit (m)	0.0	0.0	0.0
Area affected by drainage per borrow pit (m^2)	900	900	900
Total area affected by drainage around borrowpits (m^2)	0	0	0
Total volume affected by drainage around borrowpits (m^3)	0	0	0

Peat affected by drainage around turbine foundation and hardstanding	Total Exp	Total Min	Total Max	Construction Area 1 Exp	Construction Area 1 Min	Construction Area 1 Max	Construction Area 2 Exp	Construction Area 2 Min	Construction Area 2 Max	Construction Area 3 Exp	Construction Area 3 Min	Construction Area 3 Max	Construction Area 4 Exp	Construction Area 4 Min	Construction Area 4 Max	Construction Area 5 Exp	Construction Area 5 Min	Construction Area 5 Max
No. of turbines	9	9	9	9	9	9	0	0	0	0	0	0	0	0	0	0	0	0
Average length of turbine foundations at base (m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
Average width of turbine foundations at base(m)				25	25	25	0	0	0	0	0	0	0	0	0	0	0	0
Average depth of peat removed from turbine foundations (m)				1.3	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Average length of hard-standing at base (m)				97	97	97	0	0	0	0	0	0	0	0	0	0	0	0
Average width of hard-standing at base (m)				35	35	35	0	0	0	0	0	0	0	0	0	0	0	0
Average depth of peat removed from hard-standing (m)				1.3	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Maximum depth of drains (m)				1.3	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total length of foundation and hardstanding (m)				122	122	122	0	0	0	0	0	0	0	0	0	0	0	0
Total width of foundation and hardstanding (m)				60	60	60	0	0	0	0	0	0	0	0	0	0	0	0
Area affected by drainage of foundation and hardstanding area (m^2)	6360	6360	6360	6360	6360	6360	0	0	0	0	0	0	0	0	0	0	0	0
Total area affected by drainage of foundation and hardstanding area (m^2)	57240	57240	57240	57240	57240	57240	0	0	0	0	0	0	0	0	0	0	0	0
Total volume affected by drainage of foundation and hardstanding area (m^3)	37206	37206	37206	37206	37206	37206	0	0	0	0	0	0	0	0	0	0	0	0

Peat affected by drainage of access tracks	Total Exp	Total Min	Total Max
Floating roads			
Length of floating road that is drained (m)	0	0	0
Floating road width (m)	5.0	5.0	5.0
Average depth of drains associated with floating roads (m)	0.00	0.00	0.00
Area affected by drainage of floating roads (m^2)	0	0	0
Volume affected by drainage of floating roads (m^3)	0	0	0
Excavated Road			
Length of access track that is excavated road (m)	7200	7200	7200
Excavated road width (m)	5	5	5
Average depth of peat excavated for road (m)	1.3	1.3	1.3
Area affected by drainage of excavated roads (m^2)	216000	216000	216000
Volume affected by drainage of excavated roads (m^3)	140400	140400	140400
Rock-filled roads			
Length of rock filled road that is drained (m)	0	0	0
Rock filled road width (m)	0	0	0
Average depth of drains associated with rock filled roads (m)	0.0	0.0	0.0
Area affected by drainage of rock-filled roads (m^2)	0	0	0
Volume affected by drainage of rock-filled roads (m^2)	0	0	0
Total area affected by drainage of access track (m^2)	216000	216000	216000
Total volume affected by drainage of access track (m^3)	140400	140400	140400

Peat affected by drainage of cable trenches	Total Exp	Total Min	Total Max
Length of any cable trench on peat that does not follow access tracks and is lined with a permeable medium (eg. sand) (m)	0	0	0
Average depth of peat cut for cable trenches (m)	1.2	1.2	1.2
Total area affected by drainage of cable trenches (m^2)	0	0	0
Total volume affected by drainage of cable trenches (m^3)	0.00	0.00	0.00

Drainage around additional peat excavated	Total Exp	Total Min	Total Max
Volume of additional peat excavated (m^3)	4110.0	4110.0	4110.0
Area of additional peat excavated (m^2)	34800.0	34800.0	34800.0
Average depth of excavated peat (m)	0	0	0
Radius of area excavated (m)	105	105	105
Radius of excavated and drained area (m)	120	120	120
Total area affected by drainage (m^2)	10626	10626	10626
Total volume affected by drainage (m^3)	1255.00	1255.00	1255.00

Assumption: Area excavated is assumed to be a circle

RESULTS	Total Exp	Total Min	Total Max
Total area affected by drainage due to windfarm (m^2)	**283866**	**283866**	**283866**
Total volume affected by drainage due to windfarm (m^3)	**178861**	**178861**	**178861**

Click here to move to 5d. CO2 loss from drained peat Click here

Click here to move to Payback Time Click here

Volume of peat drained

Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

CO_2 loss due to drainage

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et al, 2008 - Final report).

Click here to move to 5. Loss of soil CO_2 Click here
Click here to move to Payback Time Click here

	Expected	Minimum	Maximum
Drained Land			
Total area affected by drainage due to wind farm construction (ha)	28	28	28
Will the hydrology of the site be restored on decommissioning?	No	No	No
Will the habitat of the site be restored on decommissioning?	No	No	No

Calculations of C Loss from Drained Land if Site is NOT Restored after Decommissioning

	Expected	Minimum	Maximum
Check Total volume affected by drainage due to wind farm (m^3)	178861	178861	178861
C Content of dry peat (% by weight)	53	20	64
Dry soil bulk density (g cm^{-3})	0.13	0.07	0.29
Total GHG emissions from Drained Land (t CO_2 equiv.)	46085	9242	123529
Total GHG Emissions from Undrained Land (t CO_2 equiv.)	43357	9242	87326

Assumption: Losses of GHG from drained and undrained land have the same proportion throughout the emission period.

Calculations of C loss from Drained Land if Site IS Restored after Decommissioning

1. Losses if Land is Drained

	Expected	Minimum	Maximum
Flooded period (days $year^{-1}$)	0	0	0
Lifetime of windfarm (years)	35	35	35
Time required for regeneration of bog plants after restoration (years)	10	5	15
Methane Emissions from Drained Land			
Check Rate of methane emission in drained soil ((t CH_4-C) ha^{-1} yr^{-1})	-0.004	-0.020	0.016
Conversion factor: CH_4-C to CO_2 equivalents	30.67	30.67	30.67
CH_4 emissions from drained land (t CO_2 equiv.)	-147	-712	717
Carbon Dioxide Emissions from Drained Land			
Check Rate of carbon dioxide emission in drained soil (t CO_2 ha^{-1} yr^{-1})	21.04	22.38	22.57
CO_2 emissions from drained land (t CO_2)	26878	25409	32028
Total GHG emissions from Drained Land (t CO_2 equiv.)	26732	24698	32745

Assumption: The drained soil is not flooded at any time of the year.

Note:Conversion = (23 x 16/12) = 30.67 CO_2 equiv. $(CH_4\text{-}C)^{-1}$

2. Losses if Land is Undrained

	Expected	Minimum	Maximum
Flooded period (days $year^{-1}$)	178	178	178
Lifetime of windfarm (years)	35	35	35
Time required for regeneration of bog plants after restoration (years)	10	5	15
Methane Emissions from Undrained Land			
Check Rate of methane emission in undrained soil ((t CH_4-C) ha^{-1} yr^{-1})	0.00	-0.02	0.16
Conversion factor: CH_4-C to CO_2 equivalents	30.67	30.67	30.67
CH_4 emissions from undrained land (t CO_2 equiv.)	-131	-712	3802
Carbon Dioxide Emissions from Undrained Land			
Check Rate of carbon dioxide emission in undrained soil (t CO_2 ha^{-1} yr^{-1})	18.48	22.38	4.24
CO_2 emissions from undrained land (t CO_2)	25280	25409	19346
Total GHG Emissions from Undrained Land (t CO_2 equiv.)	25150	24698	23149

Note:Conversion = (23 x 16/12) = 30.67 CO_2 equiv. $(CH_4\text{-}C)^{-1}$

3. CO_2 Losses due to Drainage

	Expected	Minimum	Maximum
Total GHG emissions from drained land (t CO_2 equiv.)	46085	9242	123529
Total GHG emissions from undrained land (t CO_2 equiv.)	43357	9242	87326
RESULTS			
Total GHG emissions due to drainage (t CO_2 equiv.)	**2728**	**0**	**36203**

Click here to move to 5. Loss of soil CO_2 Click here
Click here to move to Payback Time Click here

CO_2 loss due to drainage

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et al, 2008 - Final report).

Emission rates from soils

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Click here to move to 5d. Click here
Click here to move to Payback Time Click here

Selected Methodology = Site specific (required for planning applications)
Type of peatland = Acid Bog

Calculations following IPCC default methodology

Emission characteristics of acid bogs (IPCC, 1997)	Expected	Minimum	Maximum
Flooded period (days $year^{-1}$)	178	178	178
Annual rate of methane emission (t CH_4-C ha^{-1} yr^{-1})	0.04015	0.04015	0.04015
Annual rate of carbon dioxide emission (t CO_2 ha^{-1} yr^{-1})	35.2	35.2	35.2

Emission characteristics of fens (IPCC, 1997)	Expected	Minimum	Maximum
Flooded period (days $year^{-1}$)	169	169	169
Annual rate of methane emission (t CH_4-C ha^{-1} yr^{-1})	0.219	0.219	0.219
Annual rate of carbon dioxide emission (t CO_2 ha^{-1} yr^{-1})	35.2	35.2	35.2

Selected emission characteristics (IPCC, 1997)	Expected	Minimum	Maximum
Flooded period (days $year^{-1}$)	178	178	178
Annual rate of methane emission (t CH_4-C ha^{-1} yr^{-1})	0.04015	0.04015	0.04015
Annual rate of carbon dioxide emission (t CO_2 ha^{-1} yr^{-1})	35.2	35.2	35.2

Assumption: The period of flooding is taken to be 178 days yr^{-1} for acid bogs and 169 days yr^{-1} based on the monthly mean temperature and the lengths of inundation (IPCC, 1997, Revised 1996 IPCC guidelines for national greenhouse gas inventories, Vol 3, table 5-13)

Assumption: The CH_4 emission rate provided for acid bogs is 11 (1-38) mg CH_4-C m^{-2} day^{-1} x 365 days; and for fens is 60 (21-162) mg CH_4-C m^{-2} day^{-1} x 365 days (Aselmann & Crutzen ,1989. J.Atm.Chem. 8, 307-358)

Assumption: CO_2 emissions on drainage of organic soils for upland crops (e.g., grain, vegetables) are 3.667x9.6 (7.9-11.3) t CO_2 ha^{-1} yr^{-1} in temperate climates (Armentano and Menges, 1986. J. Ecol. 74, 755-774).

Calculations following ECOSSE based methodology

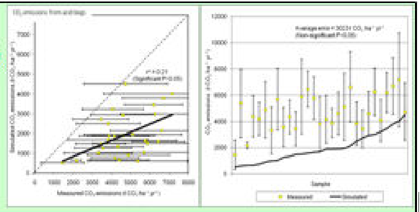
Drained Land	Expected	Minimum	Maximum
Total area affected by drainage due to wind farm construction (ha)	28	28	28
Total volume affected by drainage due to wind farm construction (m^3)	178861	178861	178861

Soil Characteristics that Determine Emission Rates	Expected	Minimum	Maximum
Average annual air temperature at the site (^oC)	9.27	4.6	15
Average water table depth at site (m)	0.50	1.00	0.10
Average water table depth of drained land (m)	0.63	1.00	0.63

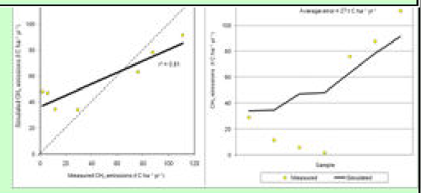
Annual Emission Rates following site specific methodology

	Expected	Minimum	Maximum
Acid bogs			
Rate of carbon dioxide emission in drained soil (t CO_2 ha^{-1} yr^{-1})	21.04	22.38	22.57
Rate of carbon dioxide emission in undrained soil (t CO_2 ha^{-1} yr^{-1})	18.48	22.38	4.24
Rate of methane emission in drained soil ((t CH_4-C) ha^{-1} yr^{-1})	-0.004	-0.020	0.016
Rate of methane emission in undrained soil ((t CH_4-C) ha^{-1} yr^{-1})	0.00	-0.02	0.16
Fens			
Rate of carbon dioxide emission in drained soil (t CO_2 ha^{-1} yr^{-1})	60.88	61.89	64.10
Rate of carbon dioxide emission in undrained soil (t CO_2 ha^{-1} yr^{-1})	55.17	61.89	10.58
Rate of methane emission in drained soil ((t CH_4-C) ha^{-1} yr^{-1})	-0.003	-0.007	0.001
Rate of methane emission in undrained soil ((t CH_4-C) ha^{-1} yr^{-1})	0.00	-0.01	0.21

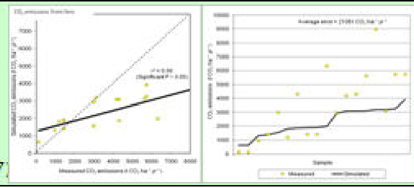
Note: Carbon dioxide emissions from acid bogs. Equation derived by regression analysis against 60 measurements (Nayak et al, 2009). The equation derived was
R_{CO2} = (3.667/1000) x ((6700 x exp(-0.26 x exp(-0.0515 × ((*W*x100)-50)))) + ((72.54 × *T*) - 800))
where R_{CO2} is the annual rate of CO_2 emissions (t CO_2 $(ha)^{-1}$ yr^{-1}),
T = average annual peat temperature (°C) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 =0.53 *P* > 0.05).
Evaluation against 29 independent experiments shows a significant association (r^2 = 0.21; P>0.05) and an average error of 3023 t CO_2 ha^{-1} yr^{-1} which is non-significant (P<0.05) (Smith et al, 1997).



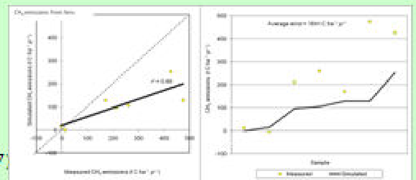
measurements (Nayak et al, 2009). The equation derived was
R_{CH4} = (1/1000) x (500 × exp(-0.1234 × (Wx100)) + ((3.529 × *T*) - 36.67))
where R_{CH4} is the annual rate of CH_4 emissions (t CH_4-C $(ha)^{-1}$ yr^{-1}),
T = average annual air temperature (°C) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 = 0.54, *P* > 0.05).
Evaluation against 7 independent experiments shows a significant association (r^2 = 0.81; P>0.05) and an average error of 27 t CH_4-C ha^{-1} yr^{-1} (significance not defined due to lack of replicates - Smith et al, 1997).



Note: Carbon dioxide emissions from fens. Equation derived by regression analysis against 44 measurements (Nayak et al, 2009). The equation derived was
R_{CO2} = (3.667/1000) x (16244 x exp(-0.175 x exp(-0.073 x ((*W*x100)-50)))+(153.23 x *T*))
where R_{CO2} is the annual rate of CO_2 emissions (t CO_2 $(ha)^{-1}$ yr^{-1}),
T = average annual peat temperature (°C) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 = 0.42, *P* > 0.05).
Evaluation against 18 independent experiments shows a significant association (r^2 = 0.56; P>0.05) and an average error of 2108 t CO_2 ha^{-1} yr^{-1} (significance not defined due to lack of replicates-Smith et al, 1997)



Note: Methane emissions from fens. Equation derived by regression analysis against experimental data from 35 measurements (Nayak et al, 2009). The equation derived was
R_{CH4} = (1/1000) x (-10+563.62 x exp(-0.097 x (*W* x 100))+(0.662 x *T*))
where R_{CH4} is the annual rate of CH_4 emissions (t CH_4-C $(ha)^{-1}$ yr^{-1}),
T = average annual air temperature (°C) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 = 0.41, *P* >0.05).
Evaluation against 7 independent experiments shows a significant association (r^2 = 0.69; P>0.05) and an average error of 164 t CH_4-C ha^{-1} yr^{-1} (significance not defined due to lack of replicate-Smith et al, 1997)



Selected emission characteristics following site specific methodology	Expected	Minimum	Maximum
Rate of carbon dioxide emission in drained soil (t CO_2 ha^{-1} yr^{-1})	21.04	22.38	22.57
Rate of carbon dioxide emission in undrained soil (t CO_2 ha^{-1} yr^{-1})	18.48	22.38	4.24
Rate of methane emission in drained soil ((t CH_4-C) ha^{-1} yr^{-1})	-0.004	-0.020	0.016
Rate of methane emission in undrained soil ((t CH_4-C) ha^{-1} yr^{-1})	0.00	-0.02	0.16

RESULTS

Selected Emission Rates	Expected	Minimum	Maximum
Rate of carbon dioxide emission in drained soil (t CO_2 ha^{-1} yr^{-1})	21.04	22.38	22.57
Rate of carbon dioxide emission in undrained soil (t CO_2 ha^{-1} yr^{-1})	18.48	22.38	4.24
Rate of methane emission in drained soil ((t CH_4-C) ha^{-1} yr^{-1})	-0.004	-0.020	0.016
Rate of methane emission in undrained soil ((t CH_4-C) ha^{-1} yr^{-1})	0.00	-0.02	0.16

Click here to move to 5d. CO2 loss from drained peat Click here
Click here to move to Payback Time Click here

Emission rates from soils

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Emissions due to loss of DOC and POC

Note: Note, CO_2 losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC or POC leaching

No POC losses for bare soil included yet. If extensive areas of bare soil is present at site need modified calculation (Birnie et al, 1991)

	Expected	Minimum	Maximum
Total C loss			
Gross CO_2 loss from restored drained land (t CO_2)	0	0	0
Gross CH_4 loss from restored drained land (t CO_2 equiv.)	0	0	0
Gross CO_2 loss from improved land (t CO_2)			
Degraded Bog	0	0	0
Felled Forestry	0	0	0
Borrow Pits	0	0	0
Foundations & Hardstanding	0	0	0
Gross CH_4 loss from improved land (t CO_2 equiv.)			
Degraded Bog	0	0	0
Felled Forestry	0	0	0
Borrow Pits	0	0	0
Foundations & Hardstanding	0	0	0
Conversion factor: CH_4-C to CO_2 equivalents	30.6667	30.6667	30.6667
% total soil C losses, lost as DOC	26	7	40
% DOC loss emitted as CO_2 over the long term	100	100	100
% total soil C losses, lost as POC	8	4	10
% POC loss emitted as CO_2 over the long term	100	100	100
Total gaseous loss of C (t C)	0	0	0
Total C loss as DOC (t C)	0	0	0
Total C loss as POC (t C)	0	0	0

Note: Only restored drained land included because if land is not

Assumption: DOC loss ranges between 7 - 40% of the total gaseous loss if calculated from the reported (minimum and maximum) values in Worrall 2009 and is **26%** of the total gaseous loss if calculated from the mean of reported maximum and minimum value in Worrall 2009. These DOC values are flux based on soil water concentration (i.e. 12.5 - 85.9 MgC/KM^2/yr) and not on flux at catchment outlet (i.e. 10.3 - 21.8 MgC/KM^2/yr)

Worrall, F. et al., 2009. The multi-annual carbon budget of a peat-covered catchment. *Science of The*

Assumption: In the long term, 100% of leached DOC is assumed to be lost as CO_2

Assumption: POC loss ranges between 4-10% of the total gaseous loss if calculated from the reported values and is **8%** of the total gaseous loss if calculated from the mean of reported maximum and minimum value in Worrall 2009. POC range is (7 - 22.4 MgC/KM^2/yr) (Worrall et al, 2009).

Assumption: In the long term, 100% of leached POC is assumed to be lost as CO_2

RESULTS			
Total CO_2 loss due to DOC leaching (t CO_2)	**0**	**0**	**0**
Total CO_2 loss due to POC leaching (t CO_2)	**0**	**0**	**0**
Total CO_2 loss due to DOC & POC leaching (t CO_2)	**0**	**0**	**0**
Additional CO_2 payback time of windfarm due to DOC & POC			
…coal-fired electricity generation (months)	0	0	0
…grid-mix of electricity generation (months)	0	0	0
…fossil fuel - mix of electricity generation (months)	0	0	0

Click here to move to Payback Time Click here

Emissions due to loss of DOC and POC

Note: Note, CO_2 losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC or POC leaching

No POC losses for bare soil included yet. If extensive areas of bare soil is present at site need modified calculation (Birnie et al, 1991)

Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

	Expected	Minimum	Maximum
Emissions due to forestry felling			
Area of forestry plantation to be felled (ha)	11.25	11.25	11.25
Carbon sequestered (tC ha^{-1} yr^{-1})	3.45	3.5	3.55
Lifetime of windfarm (years)	35	35	35
Carbon sequestered over the lifetime of the windfarm (t C ha^{-1})	120.75	122.5	124.25
RESULTS			
Total carbon loss due to felling of forestry (t CO_2)	**4981**	**5054**	**5126**
Additional CO_2 payback time of windfarm due to management of forestry			
…coal-fired electricity generation (months)	33	34	33
…grid-mix of electricity generation (months)	150	154	152
…fossil fuel - mix of electricity generation (months)	73	75	74

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Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

Gains due to site improvement

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Selected Methodology = Site specific (required for planning applications)
Type of peatland = Acid Bog

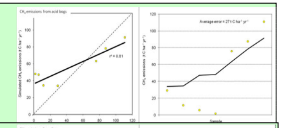
Reduction in GHG emissions due to improvement of site	**Expected result**				**Minimum result**				**Maximum result**			
Improvement of…	**Degraded Bog**	**Felled Forestry**	**Borrow Pits**	**Foundations & Hardstanding**	**Degraded Bog**	**Felled Forestry**	**Borrow Pits**	**Foundations & Hardstanding**	**Degraded Bog**	**Felled Forestry**	**Borrow Pits**	**Foundations & Hardstanding**
1. Description of site												
Period of time when effectiveness of the improvement can be guaranteed (years)	25	25	25	35	25	25	25	35	25	25	25	35
Area to be improved (ha)	0	0	0	0	0	0	0	0	0	0	0	0
Average air temperature at site (^oC)	9.27	9.27	9.27	9.27	4.6	4.6	4.6	4.6	15	15	15	15
Depth of peat drained (m)	1.30	1.30	0.00	1.30	1.30	1.30	0.00	1.30	1.30	1.30	0.00	1.30
Depth of peat above water table before improvement (m)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Depth of peat above water table after improvement (m)	0.00	0.00	0.00	1.30	0.00	0.00	0.00	1.30	0.00	0.00	0.00	1.30
2. Losses with improvement												
Flooded period (days year^{-1})	178	178	178	178	178	178	178	178	178	178	178	178
Time required for hydrology and habitat to return to its previous state on restoration (years)	0	0	0	0	0	0	0	0	0	0	0	0
Improved period (years)	25	25	25	35	25	25	25	35	25	25	25	35
Methane emissions from improved land												
Site specific methane emission from improved soil on acid bogs (t CH_4-C ha^{-1} yr^{-1})	0.496	0.496	0.496	-0.004	0.480	0.480	0.480	-0.020	0.516	0.516	0.516	0.016
Site specific methane emission from improved soil on fens (t CH_4-C ha^{-1} yr^{-1})	0.560	0.560	0.560	-0.004	0.557	0.557	0.557	-0.007	0.564	0.564	0.564	0.000
IPCC annual rate of methane emission on acid bogs (t CH_4-C ha^{-1} yr^{-1})	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
IPCC annual rate of methane emission on fens (t CH_4-C ha^{-1} yr^{-1})	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219
Selected annual rate of methane emission (t CH_4-C ha^{-1} yr^{-1})	0.496	0.496	0.496	-0.004	0.480	0.480	0.480	-0.020	0.516	0.516	0.516	0.016
CH_4 emissions from improved land (t CO_2 equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from improved land												
Site specific CO_2 emission from improved soil on acid bogs (t CO_2 ha^{-1} yr^{-1})	0.34	0.34	0.34	24.00	-0.91	-0.91	-0.91	22.76	1.86	1.86	1.86	25.52
Site specific CO_2 emissions from improved soil on fens (t CO_2 ha^{-1} yr^{-1})	5.27	5.27	5.27	64.75	2.64	2.64	2.64	62.12	8.49	8.49	8.49	67.97
IPCC annual rate of carbon dioxide emission on acid bogs (t CO_2 ha^{-1} yr^{-1})	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IPCC annual rate of carbon dioxide emission on fens (t CO_2 ha^{-1} yr^{-1})	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Selected annual rate of carbon dioxide emission (t CO_2 ha^{-1} yr^{-1})	0.34	0.34	0.34	24.00	-0.91	-0.91	-0.91	22.76	1.86	1.86	1.86	25.52
CO_2 emissions from improved land (t CO_2)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from improved land (t CO_2 equiv.)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**
3. Losses without improvement												
Flooded period (days year^{-1})	0	0	0	0	0	0	0	0	0	0	0	0
Time required for hydrology and habitat to return to its previous state on restoration (years)	0	0	0	0	0	0	0	0	0	0	0	0
Improved period (years)	25	25	25	35	25	25	25	35	25	25	25	35
Methane emissions from unimproved land												
Site specific methane emission from unimproved soil on acid bogs (t CH_4-C ha^{-1} yr^{-1})	0.496	0.496	0.496	0.496	0.480	0.480	0.480	0.480	0.516	0.516	0.516	0.516
Site specific methane emission from unimproved soil on fens (t CH_4-C ha^{-1} yr^{-1})	0.560	0.560	0.560	0.560	0.557	0.557	0.557	0.557	0.564	0.564	0.564	0.564
IPCC annual rate of methane emission on acid bogs (t CH_4-C ha^{-1} yr^{-1})	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
IPCC annual rate of methane emission on fens (t CH_4-C ha^{-1} yr^{-1})	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Selected annual rate of methane emission (t CH_4-C ha^{-1} yr^{-1})	0.496	0.496	0.496	0.496	0.480	0.480	0.480	0.480	0.516	0.516	0.516	0.516
CH_4 emissions from unimproved land (t CO_2 equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from unimproved land												
Site specific CO_2 emission from unimproved soil on acid bogs (t CO_2 ha^{-1} yr^{-1})	0.34	0.34	0.34	0.34	-0.91	-0.91	-0.91	-0.91	1.86	1.86	1.86	1.86
Site specific CO_2 emissions from unimproved soil on fens (t CO_2 ha^{-1} yr^{-1})	5.27	5.27	5.27	5.27	2.64	2.64	2.64	2.64	8.49	8.49	8.49	8.49
IPCC annual rate of carbon dioxide emission on acid bogs (t CO_2 ha^{-1} yr^{-1})	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
IPCC annual rate of carbon dioxide emission on fens (t CO_2 ha^{-1} yr^{-1})	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
Selected annual rate of carbon dioxide emission (t CO_2 ha^{-1} yr^{-1})	0.34	0.34	0.34	0.34	-0.91	-0.91	-0.91	-0.91	1.86	1.86	1.86	1.86
CO_2 emissions from unimproved land (t CO_2)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO_2 equiv.)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**
RESULTS **4. Reduction in GHG emissions due to improvement of site**												
Total GHG emissions from improved land (t CO_2 equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO_2 equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Reduction in GHG emissions due to improvement (t CO_2 equiv.)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**
Additional CO_2 payback time of windfarm due to site improvement												
…coal-fired electricity generation (months)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**
…grid-mix of electricity generation (months)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**
…fossil fuel - mix of electricity generation (months)	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**	**0**

Click here to move to Payback Time Click here

Gains due to site improvement

Note: Note, CO_2 losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al, 2008 - Final report).

Note: Methane emissions from acid bogs. Equation derived by regression analysis against 57 measurements (Nayak et al, 2009). The equation derived was
R_{CH4} = (1/1000) x (500 × exp(-0.1234 × (Wx100)) + ((3.529 × T) - 36.67))
where R_{CH4} is the annual rate of CH_4 emissions (t CH_4-C (ha)$^{-1}$ yr^{-1}),
T = average annual air temperature (^oC) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 = 0.54, P > 0.05).
Evaluation against 7 independent experiments shows a significant association (r^2 = 0.81; P>0.05) and an average error of 27 t CH_4-C ha^{-1} yr^{-1} (significance not defined due to lack of replicates - Smith et al, 1997).



Note: Methane emissions from fens. Equation derived by regression analysis against experimental data from 35 measurements (Nayak et al, 2009). The equation derived was
R_{CH4} = (1/1000) x (-10+563.62 x exp(-0.097 x (W x 100))+(0.662 x T))
where R_{CH4} is the annual rate of CH_4 emissions (t CH_4-C (ha)$^{-1}$ yr^{-1}),
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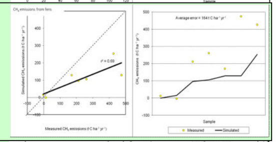
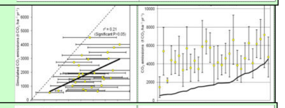
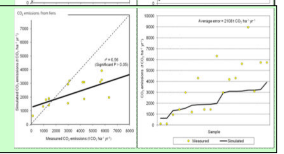


R_{CO2} = (3.667/1000) x ((6700 x exp(-0.26 x exp(-0.0515 × ((Wx100)-50)))) + ((72.54 × T) - 800))
where R_{CO2} is the annual rate of CO_2 emissions (t CO_2 (ha)$^{-1}$ yr^{-1}),
T = average annual peat temperature (^oC) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 =0.53 P > 0.05).
Evaluation against 29 independent experiments shows a significant association (r^2 = 0.21; P>0.05) and an average error of 3023 t CO_2 ha^{-1} yr^{-1} which is non-significant (P<0.05) (Smith et al, 1997).



Note: Carbon dioxide emissions from fens. Equation derived by regression analysis against 44 measurements (Nayak et al, 2009). The equation derived was
R_{CO2} = (3.667/1000) x (16244 x exp(-0.175 x exp(-0.073 x ((Wx100)-50)))+(153.23 x T))
where R_{CO2} is the annual rate of CO_2 emissions (t CO_2 (ha)$^{-1}$ yr^{-1}),
T = average annual peat temperature (^oC) and
W is the water table depth (m).
The equation shows a significant correlation with measurements (r^2 = 0.42, P > 0.05).
Evaluation against 18 independent experiments shows a significant association (r^2 = 0.56; P>0.05) and an average error of 2108 t CO_2 ha^{-1} yr^{-1} (significance not defined due to lack of replicates-Smith et al, 1997)



Note: Methane emissions from acid bogs. As above

Note: Methane emissions from fens. As above

Note: CO_2 emissions from acid bogs. As above

Note: CO_2 emissions from fens. As above

TII CARBON TOOL

Ch 15: Material Assets, Table 15-7					Distance Assumptions	TII Embodied Carbon Tool Inputs (https://web.tii.ie/index.html)						TII Transport Inputs (https://web.tii.ie/index.html)		
Material	Total no. Truck Loads	Truck Types	TII Embodied Carbon	TII Traffic	Distance (km)	Category	Sub-Category	Material	Quantity	Unit	Embodied tCO2e	Transport Type	Distance (km)	Transport TCO2e
Concrete	963	Concrete mixers	✓	✓	17.4	Series 1700 Structural Concrete	Concrete - Construction General	Construction - Standard Mix (Average)	18,489,600	kg	1911.09	HGV - Rigid - Average	16756.2	20.5118
Delivery of plant	35	Large artic		✓	96.85							HGV- All - Average	3389.75	3.6762
Fencing & gates	3	Large artic		✓	17.4							HGV- All - Average	52.2	0.0566
Compound setup	36	Large artic		✓	17.4							HGV- All - Average	626.4	0.6793
Steel	24	Large artic	✓	✓	96.85	Other	Structural Steelwork	Anchorages and holding down bolt assemblies	480	tonnes	860.69	HGV- All - Average	2324.4	2.5208
Rock and stone	14450	Truck	✓	✓	17.4	Series 2400 - Brickwork, Blockwork and Stonework	Brickwork and Blockwork	General Stone	289,000.00	tonnes	22831	HGV - Rigid - Average	251430	258.3594
Ducting and cabling (internal)	264	Large artic		✓	17.4							HGV- All - Average	4593.6	4.9818
Tree felling	17	Large artic		✓	96.85							HGV- All - Average	1646.45	1.7856
Crane (to lift steel)	1	Large artic		✓	96.85							HGV- All - Average	96.85	0.105
Substation	100	Large artic		✓	17.4							HGV- All - Average	1740	1.887
BESS	100	Large artic	✓	✓	17.4							HGV- All - Average	1740	1.887
Cranes for turbines	12	Large artic		✓	17.4							HGV- All - Average	208.8	0.2264
Refuelling for plant	186	Large artic		✓	17.4							HGV- All - Average	3236.4	3.5099
Site maintenance	135	Large artic		✓	17.4							HGV- All - Average	2349	2.5475
Miscellaneous	90	Large artic		✓	17.4							HGV- All - Average	1566	1.6983
Total											25,602.78			304.43

List of Assumptions

Embodied Carbon Assumptions		
Item	Description	Assumption
Volume of Concrete Mixer	Calculation completed based on the average concrete mixer holding 8m3 of concrete	8
Volume of Average Artic Truck	Calculation completed based on the average artic truck having a carrying capacity of 20 tonnes	20
Ducting and cabling (internal)	Embodied carbon of electrical equipment not included as an option in TII Carbon Tool	-
Grid connection cable laying	Embodied carbon of electrical equipment not included as an option in TII Carbon Tool	-
Tree Felling	Embodied carbon of tree felling is included in the Macauley Institute Carbon Calculator for Wind Farms on Peatland	-
Turbine Lifecycle	Embodied carbon of the overall turbine lifecycle is included in the Macauley Institute Carbon Calculator for Wind Farms on Peatland	-
Concrete	Concrete will be required for various elements of the Proposed Project Approximately 7,704m3 of material is assumed to be required based on 963 concrete mixers being required, assumed 8m3 carrying capacity, and assumed density of 2400kg/m3 The TII Carbon tools requires units in kg for this material type, therefore the following calculation was completed: -7,704m3 * 2400kg/m3 = 20,412,000kg	18,489,600.00
Steel	Steel will be required for various elements of the Proposed Project. Approximately 480 tonnes of steel is assumed to be required based on 24 trucks being required and an assumed carrying capacity of 20 tonnes	480.00
Rock and Stone	Rock and Stone will be required for various elements of the Proposed Project. Approximately 289,000 tonnes of rock/stone is assumed to be required based on 14,450 trucks being required and an assumed carrying capacity of 20 tonnes	289,000.00

Please note that the assumptions for the embodied carbon and traffic assumptions are made based on best estimates of material sources. In reality the location of material sources will be dependent on what is available at the time of construction. The implications of distance variations on the estimation for carbon calculations is of a very low magnitude within the context of the overall carbon calculations and considered appropriate for the purposes of assessment in the EIAR.

Traffic Assumptions		
Item	Description	Assumption
Import (P) Distance	For modelling purposes, the average distance from Shannon Foynes Port and the Port of Galway for transport of all other materials for the site	96.85
Quarry (Q) Distance	As outlined in Section 4.5.3 of Chapter 4 of the EIAR 3 no. quarries have been identified within 20km for the purposes of delivering material to the Proposed Project site. An average distance of the construction haul routes has been used for modelling purposes.	17.4
Truck Emissions Factor	Calculated from an HGV - Rigid - Average emission factor as provided in the TII Carbon Tool. Source: 2024 DEZNZ emission factors - 'Delivery vehicles' tab, All Rigids HGVs and used Average laden weight. 2024 DEZNZ emission factors - 'WTT - delivery vehicles & freight' tab, all Rigids HGVs and used Average laden weight.	1.02756
Large Artic Emission Factor	Calculated from an HGV - All - Average emission factor as provided in the TII Carbon Tool. Source: 2024 DEZNZ emission factors - 'Delivery vehicles' tab, All HGVs and used Average laden weight. 2024 DEZNZ emission factors - 'WTT - delivery vehicles & freight' tab, all HGVs and used Average laden weight.	1.0845

Truck Emissions Factor	Calculated from an HGV - Articulated - Average emission factor as provided in the TII Carbon Tool	1.30212

Please note that the assumptions for the embodied carbon and traffic assumptions are made based on best estimates of material sources. In reality the location of material sources will be dependent on what is available at the time of construction. The implications of distance variations on the estimation for carbon calculations is of a very low magnitude within the context of the overall carbon calculations and considered appropriate for the purposes of assessment in the EIAR.

Carbon Fixing Vegetation Assumptions		
Item	Description	Assumption
Calculation of Carbon Storage Potential in Enhancement Measures	The carbon storage capacity of restored habitats will vary over time as vegetation matures and land use and the baseline environment change. Therefore, while it can be assumed that native woodland replanting and enhancement of wet heath habitat on the Site will result in an increased capacity of carbon storage due to the carbon storage potential that exists within these habitats , to ensure the assessment below is identified under a theoretical precautionary scenario the quantification of these potential carbon savings (via an increase in carbon storage potential) associated with these measures has not been included in the carbon savings assessment. Please note, the carbon sequestration potential associated with the replanting of native woodland will be able to be determined in the future via the Teagasc Forest Carbon Tool ; currently this is not able to be completed due to Teagasc carrying out further analysis and validation on current data and the sequestration potential not being available in the public domain.	Not considered in assessment or quantified
Calculation of Carbon Loss from removal of carbon fixing vegetation	Carbon losses associated with the removal of other carbon-fixing vegetation will result in additional carbon losses. These have not been quantified as the lack of consistent national-level field data and methodologies limits the ability to make accurate projections on carbon sequestration potential for other carbon fixing habitat types, i.e., hedgerow, grassland, etc., and therefore carbon loss associated with removal. While it can be assumed that loss of carbon fixing vegetation will occur as part of the Proposed Project due to the removal of these habitat types, the exact carbon loss is not quantifiable.	Not considered in assessment or quantified